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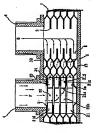
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#### (54) PLATE TYPE HEAT EXCHANGER

## (57)Abstract:

PROBLEM TO BE SOLVED: To improve remarkably and surely the total heat transfer performance of a refrigerant in two-phase flow of gas and liquid in a fluid flow passage for the refrigerant between laminated heat transfer plates. SOLUTION: In a heat exchanger, hollow members 21 are fixed to the inlet flow passages 5a of fluid flow passages 5 for refrigerant which are formed between a plurality of heat transfer plates 1 to conduct the refrigerant P of two-phase flow of gas and liquid to flow into the fluid passages 5 through the hollow members 21. The refrigerant P is introduced into an internal space 23 from the fore stage small holes 22 of inner wall parts 21a of the hollow members 21 after choking the same to evacuate and expand the same. In this case, an initial uniform distribution of gas phase and liquid phase of the refrigerant P as well as the subdivision of the gas phase are effected, then, the uniform distribution of the gas phase and the liquid phase as well as the subdivision of the gas phase are effected when the refrigerant P is passed from the internal space 23 into the rear stage small holes 23 of an external wall part 21b to introduce the same into the fluid flow passages 5, whereby the total heat transfer performance of the refrigerant P in the fluid flow passages 5 is improved surely.



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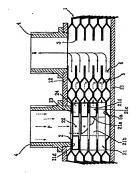
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## (54) 【発明の名称】 プレート式熱交換器

#### (57)【要約】

【課題】 積層された伝熱プレート間の冷媒用流体流路 における気液二相流の冷媒のトータルの伝熱性能を顕著 に確実に向上させる。

【解決手段】 複数の伝熱プレート1の間に形成された 冷媒用流体流路5の入口流路5aに中空部材21を固設 して、中空部材21を通して気液二相流の冷媒Pを流体 流路5に流出させる熱交換器で、中空部材21の内壁部 21aの前段小孔22から冷媒Pを絞って内部空間23 に流入させて減圧膨張させ、このときに初回の冷媒Pの 気相と液相の均一分配と気相の細分化を行い、内部空間 23から外壁部21bの後段小孔23に冷媒Pを通過さ せて流体流路5に流出させるときも気相液相の均一分配 と気相の細分化を行うようにして、冷媒Pの流体流路5 におけるトータル伝熱性能を確実に向上させる。



## (2) 001-280888 (P2001-(.88

#### 【特許請求の範囲】

【請求項 1】 精層された複数の伝統プレートの間に、 一方が気流ニ相流冷媒である2種の流体が流通して熱交 技が行われる流体流路を交互に形成し、伝統プレートに 形成した冷媒の入口用通路孔周辺の入口流路から冷媒用 流体流路に倍媒を流入させるプレート式熱交換器におい て、

冷健用液体流路の入口流路に、外部からの気液二相流冷 線がその流力が安られて流入し施散して流出する原料・ 入及び、この原例・刊を選出した冷盤が発出距離する 内部空間、及び、この内部空間で減圧耐寒した冷盤がそ の流れが絞られて流入し拡散して流出する後別・引を する中空部分を超でし、この中空部列の後別・引から 無用液体液路に冷盤を流入させることを特徴とするプレ トル本学や海径・

[請求項2] 中空部材が円筒状の小径の内壁部とこの 内壁部より大径の外壁部を有するリング状で、内壁部に 前段小孔を、外壁部に後段小孔を、内壁部と外壁部の間 に内部空間を形成したことを特徴とする請求項1記載の プレート式無交換器。

【請求項3】 中空部材を開接する伝熱プレートでろう 材を介して挟持させて、伝熱プレート間にろう付け固定 したことを特徴とする請求項1又は2記載のプレート式 映安強器。

#### 【発明の詳細な説明】

#### [0001]

【発明の属する技術分野】本発明は、複数枚の伝熱プレートをろう付け等で積層一体化したプレート式熱交換器 に関する。

#### [0002]

【経本分技術】冷蔵機のフロン等の冷謀は、蒸発が必然 交換器から100%気体となって圧縮機から振縮計に送 られて温度上昇した液体となり、この液体が膨緩力体 程膨緩して急激に温度低下した液相(液体)と気相(気 協)の混合した気値、相談となって源光器の無交換器は 送られる循環サイタルで恒少的に利用される。一のよう な心産療の冷燥の原発器に用いられる無交換器は、複数 がの応急プレントを掲層一体化したプレート式蒸突換器 が一般的であり、その基本構造例を図7及び図8に示 し、これを改変した無交換器を図り及び図10で説明す も、

【0003】図7に示される無交換器は、複数枚の伝統 プレート1と2枚の金属フレーム12、13をろう材 (図示せず)を介し模層して、高温・美空下でろう付け (ブレージング)したブレージング式無交換器である。 伝熱プレート1と金属フレーム12、13はステレンス 製の権矩形板で、各伝然ブレート104異部に蒸焚機されるぐき2種の流体の通路代え2、3が形成され、一方の 金属フレーム12の4層部に2種の流体の出入口となる メズル4が真遇させてろう付けされる。

【0004】伝熱プレート1は波板プレートの熱交換伝 熟部1aと、熱交換伝熱部1aの周縁部を折曲した縁立 て部1bを有し、隣接する伝熱プレート1の縁立て部1 bが気密にろう材で溶融接合される。複数の伝熱アレー ト1を積層一体化したとき、各々の熱交換伝熱部1aの 4隅に形成された通路孔2、3が同心に対向して連通す る。また、複数の伝熱プレート1を積層一体化したと き、図8に示すように各伝熱プレート1間に一方が冷媒 である2種の液体が溶消する液体溶路5.6が交互に形 成される。図8は1種の流体である気液二相流の冷媒P の入口側と他の1種の流体Qの出口側の断面が示され、 冷媒用流体流路5の冷媒用通路孔2の周辺部通路が冷媒 用入口流路5aである。冷媒用入口流路5aは、隣接す る伝熱プレート1の相互にろう付けされた入口側通路孔 2の周辺部で囲まれたリング状の空間部分で、冷媒用入 口側通路孔 2と連通するノズル4 に外部から流入した冷 媒Pは、入口側通路引、2から入口流路5aに入り、入口 流路5aから流体流路5を流通して隣りの流体流路6を 流通する他の流体Qを冷却する。

【0005】冷媒用流体溶除5の入口流降5aに流入す る冷媒Pは、図示しない凝縮器で凝縮された液体を散現 弁で製張させて急冷させた液相と気相の気液二相流冷媒 であり、この気液二相流冷謀の液相と気相が分裂と合体 を繰り返して流体流路5を流れる。流体流路5を流れる 冷媒Pのトータル伝熱性能を高く確保するため、入口液 器5aから流体流路5に入る冷葉Pの気相と溶相の均一 分配と、熱伝導率の悪い池状の気相の細分化が促進され るように、入口流路5 aの形状やサイズが設計される。 しかし、隣接する伝熱プレート1間の隙間だけの入口流 路5aでは冷媒Pが単に通過するだけであるので気相と 液相の均一分配や気相の細分化を促進する機能に劣り、 1つの流体流路5における冷媒Pのトータル伝熱性能が 低くならざるを得ない。そこで、この低い伝熱性能を見 越して伝熱プレート1の枚数を増やし、冷媒用流体流路 5の数を増やして冷媒のトータルの低伝熱性能をカバー するようにしているが、これでは熱交換器が大型化し、 コスト高となる。

【00061 熱交換器の疾流 一視流冷寒 アゥトーテルの 低気整性能を伝整プレート数を増大させることなくが、 一するため、例えば図りに示すプレート式急交換器で は、冷解用人口認鳴ちぁに図10に示すようを薄痕の金 限リング14 を認定している。金周リング14はテンレス、網あるいは紫髪の厚板で、内周面から外原面に貫 直させて1条のトンネル孔15を有する。毎別ング14 4の時程は伝数プレート10冷採用温熱孔2と同一か、 それよりも小さく、外径は連料孔2より大きい、金線リング14 以外214 に関連する任無プレート1間に挟持され、連絡 孔2と同心に位置決めして固定される。トンネル孔15 は、気能工程域の冷葉 戸が収られて流入し、鉱散して流 出する6階を1ma程度の分析であり、 !(3) 001-280888 (P2001-4>88

【0007】図9の熱交換線においては、冷媒用人口調 通路孔2に流入した気矩二相流冷煤Pが金属リング14 の内周のトンネル孔入口に炭をれて流入し、トンネル孔 15を変動して金属リング14外周のトンネル孔出口から舷液活出して冷媒用流体連路5を流動する。このよう も配放。実施工相流の冷煤Pが小引のトンネル孔15を過ぎる間に、実施工相流の冷煤Pが小引のトンネル孔15を過ぎる間に、実施工相流の冷煤Pの比較対大きを位径の気相 (気泡)が小さを対抗に個が化され、かつ、気相と液相 の流れが切られ能散されることで均一分配化されるよう にして、冷媒用が体出れる際の冷域Pのトータル径性体が高くなるようにして、おり、100円の

#### 180001

【発明が解決しようとする課題】図9の熱交換器は、金 犀リング14による気液<sup>一</sup>相流冷媒Pの均一分配。気相 の細分化の性能が良ければ、冷媒Pのトータル伝熱性能 が上がって伝熱アレート数を少なくして熱交換器の小型 低コスト化が実現されるのであるが、未だ金属リング 14による題等を性能改善が果たされていないのが現状 である。その要因として、金属リング14の1箇所のト ンネル孔15に気液二相流冷媒Pを通過させるだけでは 気相の細分化が不十分であり、不均一で大きな気相が流 体流路5を流れる可能性が大であり、このことがトータ ル伝熱性能の顕著な改善を難しくしている。また、金属 リング14のトンネル孔15の内径を縮小したり、トン ネル孔数を増やして、トータル伝熱性能の改善策とする ことも行われているが、その改善効果が不十分であっ て、伝熱プレート数を少なくして熱交換器の小型・低コ スト化を実現させることが難しいのが現状である。

【0009】本発明は図9の無交換器の問題点に鑑みてなされたもので、その目的とするところは、気液工相流 待媒のトークル伝熱性能を顕著に確実に改善し得たアレート式無交換器を提供することにある。 【0010】

【課題を解決するための手段】本発明の上記目的を通成する請求項1の形明法、精関者れた複数の伝統アレートの間に、一方が成在 相談神をするると覆の流体が充通して無実動が行われる流体流線を交互に形成し、伝統アレートに形成した冷線の入口用温路孔用辺の入口流路へ合線展所成流線に冷線を流入させるアレート式無交換器において、冷線解形成体流路の入口流路に、外部からの家海二根流冷線がその流れが安られて流入比較して流出する前段外形。及び、この内部空間で延圧解析、近圧解はする内部空間、及び、この内部空間で延圧解析、近上常線が全の流れが役られて近入上散散して流出する接段小孔を有する中空部材を配置し、この中空部材の接段小孔から冷線用流体流路に冷線を流入上散して流出する。

【0011】ここで、中空部材は冷媒用流体流路の入口 流路を塞ぐリング状等の金属箱、金属容器で、伝熱プレ ートにろう付けや溶接等で固定される。この中空部材 は、冷媒流れに対して上流側に前段小孔を下流側に後段 小孔を有し、この前後段の小孔の間に内部空間が形成さ れて、気液二相流の冷媒は前段小孔から内部空間を通っ て最終的に後段小孔から流体流路に流出して行く。中空 部材の前段と後段の各小孔は単一孔、或いは、複数孔が 可能であり、これら小孔の内径、孔中心線の角度も任意 で有り、熱交換器の種類に応じて適宜に設定される。ま た、中空部材の内部空間は単一空間、或いは、仕切壁で 流体流れ方向直列に仕切られた複数空間であってもよ く、この複数空間の場合は複数空間を仕切る仕切壁に中 間的な小孔を形成して複数空間に冷媒を順に流すように する。気液二相流の冷媒が複数の小孔を絞られて流通 し、さらに、小孔から内部空間に減圧膨張して流出する といった異なる形態の冷媒流流が複数同に百り段階的 繰り返し的に行われることで、気液二相流冷媒の最終的 な気相と液相の均一分配、気相の細分化が確実に顕著に 行われる。

[0012] 本発明の講求項2の発明は、中空解析が円 病状の小径の内盤部とこの内盤部より大陸の外型部を有 するリング状で、内壁部に関係小机を、外型部に接が、 孔を、内壁部と外盤部の間に内部空間を形成したことを 特徴とする。このリング状中型が分析が従来が の一直発育した形で間接される。伝統プ レートの作成入口流路孔に成人と心性がリング状中空 部材の内壁部の中を通治する間に冷域の一部が削負小孔 に流入する。

[0013] 本売得の請求項3の発明は、中空部材を開 读する低熱プレートでろう材を介して供許させて、伝熱 プレート間にろう付け面定したことを特徴とする。この ように中空部材を伝熱プレートにろう付けするようにす さと、推動の伝統プレートとろう付けするようにす 式洗支換器の製作率に、接数の伝熱プレートのろう付け と同一工程で中空部材のろう付けができて、然支換器の 製作が工器が、コスト的に本材に未致能力る。

#### [0014]

【発明の実施の形態】以下、本発明の実施形態を図1万至図6を参照して詳述する。なお、この実施形態は図8 や図9の熱交換器に適用したもので、図1万至図6の図 7万至図9と同一、又は、相当部分には同一参照符号を 付して、その詳細説明は省略する。

[0015] 図1に示される第1の実施器の然之地話はブレージング式のアレート式奈交換製で、推散の伝統アレート1の間に形成された複数の作鬼用流体流路5の人口温路5 aの4を4に完盛材21を図影している。中空部材21は図3に示すようなリング状のステンレス等の金属製品で、円筒状の内壁第21aと外量部21bを有し、内壁部21aの例えば1箇所に前段小孔22が、外壁部21bの1箇所に後別小孔24が販され、内壁部21aと外壁部21bの4間が再数分前を配置23が

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形成される。前後段の各小孔22,24は、気液二相流 の冷媒Pが絞られて流通する内径2mm程度の貫通孔で ある。

[0016]図1及2回31元宗たち中空総材21は、 その内量部21aが伝統アレート1の冷葉用入口流路孔 2の内径より小さ公円高状であり、外壁部21aと外壁部 25分型部21bの下端がリング状態疾部21cで一株に 連結される。この内壁部21aと外壁部21bと底板部 21cで構成される上端間ロリング状容器の上し底板部 21cで構成される上端間ロリング状容器の上の大変 21cで構成される上端間ロリング状容器の上の大変 21cで構成される上端間ロリング状容器の上の 21が構成される。整板21dは、東流工程成の冷緩P が前段/孔22を辿らず世末少円が整定の2は元が のを組止する空間密用液であり、このような繋ば辺2の 第2の実施形態においては不必要で省略してあり、その 理由は接続する。そ

【0017]リング共中空部材21は、陽終する伝熱アレート1の冷謀用入口流路孔2の中心後と内壁部21名の中心後と内壁部21名の中心後と内壁部21名の中心後と内壁部21名の中心後と内壁部21名の中心後が127~3分である。 の生かられて固定、例えばちう付けらて固定される。このように中空部材21を伝統アレート同士の5う付けら中空が材21の方付けるアレージング式数交換部の製作時に伝統アレート同士の5う付けと中空が材21の5)付けが11至の実行できて、アレージング式数交換器の製作が工程的、コスト的に有利となる。 冷謀用入口流路5aにリング状中空部材21は、その後 段小元2名を治理形弦体部85の方向に向けて固定される。この中空部材21の前段小孔2名である。

【0018】複数の伝熱アレート1間の複数の冷媒用入 口流路5 aに複数のリング状中空部材21を固定して、 冷媒入口ノズル4から気液二相流冷媒Pを流入させる と、冷媒Pは各リング状中空部材21の内壁部21a内 周面を軸方向に流動し、一部の冷媒Pが内壁部21aの 前段小孔22に絞られて内部空間23へと流入する。こ の冷媒流入は、図5に示すように行われる。内壁部21 aの外を流動する気液二相流の冷媒Pは、図5の実線矢 印の概念図で示される液相P1と図5の粒子概念図で示 される気相(気泡)P2であり、気相P2の粒径が比較 的大きく、仮にこれをそのまま冷媒用流体流路5に流入 させると伝熱性能が低下するが、本発明においてはまず 液相P1と気相Pを前段小孔22から内部空間23に流 入させる。前段小孔22に粒径の大きな気相P2が通過 するとき、絞られて小粒径化されると共に、前段小孔2 2から内部空間23に流出するときに減圧膨張するた め、内部空間23では気相P2と液相P1が均一分配化 され、気相P2のほとんどが小粒子状に細分化される。 【0019】さらに、前段小孔22から内部空間23に

流入した倉籍Pは、図3 (B) に示すようにリング状の 内部空間23を流動して、最終的に競扱が124に被ら れて流入して冷燥用流水流器をに流出して行く、冷峻P が後段が孔24を逃逃する段階においても気相液相の均 一分配化 気相振分化が行われる。この後段が124に も気無磁が化は、前段が122から内部空間23を流 動した比較的大きな中粒子の気相や、内部空間23を流 動する場面が低いたないた中粒子の気相が小粒子状に 細かされるたとでする。

【00201以上のように中空部村21で気流工機気冷 類甲は、前後2段の小孔22、24による2段階に亘る 気相液積のカー分配及び気和細分化と、前段小孔2か ら内障空間23への活出と後段小孔24から流水高路5つ 空間かっ流出による2段階に直め延距断段の作用で、 確実かり囲落に気相流相のお一分配と気相線分化が行わ れて高体流路5を流重する。そのため、1つの流体流路 ちたおける冷様ドのトータル伝熱性膨が確実に向上し、 伝熱アルート数を少なくして熱交換器を小型化して、低 コストで製作することが可能とる。

【0021】図6は、図1の熱交換器を治液機の冷箕領 東ナアムに週用なたときの際暗空、延縮器 (図示す かか送られてる治療は上海料 P が表達の大な C 溶相 P 20 気流 相 20 元 が R 20 元 か 20 元 が R 20 元 か 20 元

[0022] 図2に示される第2の実施影響の無交換器は、上記中空部材21の構造変更例を示すめて、図2における中空部材21 "は図4に示すような響無しの上端間14度のリング状金属写幹である。この中空部材21 は、円筒状の内盤部21aと外差部21bとリング状の接続第21cだけで構成され、内盤部21aの1箇所に前砂利、22が外型部21bの1箇所に接砂小孔24が形成され、内盤部21aと外壁部21bの局が内部空間24となる。

[0023] 図2の中空部材21'は、これが間除され 売待媒入口流路5 aの形状寸法に対応させたもので、こ の場合の冷媒入口流路5 aの冷域肝温路孔2の内容より 中空部材21'の内壁部21 aの内径が大きめに設定し である。したがって、蓋集しの中空部材21'を冷媒入 口流路5 aに位置決めして固定すると、中空部材217 の上端間口が伝金プレート1の温路孔2の周辺能で塞が

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れて内部空間23が略密閉空間となるので、この中空部 材21'は蓋板を必要としない、このような蓋無し中空 部材21 の気液二相流冷媒 Pに対する気相液相均一分 散化や気相細分化の機能は、図3の蓋有り中空部材21 と同様ゆえに説明は省略する。

【〇〇24】以上の各実施形態において中空部材をリン グ状としたが、これはリング状の冷媒用入口流路に対応 させたもので、冷媒用入口流路の形状に応じた任意の形 状とすることができ、たとえば半円弧状の中空部材等で あってもよい。また、中空部材の内壁部の1箇所に前段 小孔を、外壁部の1箇所に後段小孔を形成したが、これ ら各小孔の個数、大きさ、形状、形成位置は特定されな い。また、中空部材の内壁部と外壁部の間に1つの内部 空間を形成するようにしたが、この内部空間を複数に仕 切って、仕切られた複数の空間を冷媒が順に減圧膨張し て流動するようにしてもよい。

【0025】さらに、本発明は、ブレージング式熱交換 器以外のガスケットシール式のプレート式熱交換器等に も有効に適用されるものであり、例えばガスケットシー ル式外交換器においては中空部材を伝熱プレートに溶接 で固定、或いは、ガスケットを介して伝熱プレートに圧 接して固定するようにすればよい。

[0026] 【発明の効果】請求項1と2の発明によれば、気液二相 流の冷媒が中空部材の前段小孔、内部空間、後段小孔を 順に通過し、この通過時に少なくとも2段階に亘って気 相液相の均一分配と気相の細分化が行われて冷媒用流体 流路に流出するので、流体流路における冷媒の気相液相 均一分配と気相細分化が十分顕著に実行されて、冷媒の トータル伝染件能が向上し、熱交換効率に優れたプレー ト式熱交換器が提供できる。また、冷媒のトータル伝熱 件能の改善により、伝熱プレート数を少なくして熱交換 器を小型軽量にし、製作コストを低減させることが容易 になる.

【0027】請求項3の発明によれば、隣接する伝熱ア レート間に中空部材をろう付けで固定することで、複数 の伝熱プレートを同時にろう付けするブレージング式熱 交換器が1工程のろう付けで製作でき、また、ガスケッ

ト等の特別な別部材を使用すること無く中空部材を既存 の伝熱プレートに既存のろう付け方法で固定することが できて、製作的に有利なアレート式熱交換器が提供でき

### 【図面の簡単な説明】

- 【図1】本発明の第1の実施形態を示すプレート式熱交 機器の要部の所面図。
- 【図2】本発明の第2の実施形態を示すプレート式熱交 機器の要部の断面図。
- 【図3】(A)は図1熱交換器における中空部材の断面 図、(B)はT1-T1線の断面図。
  - 【図4】図2塾交後器における中等部材の断面図。
  - 【図5】図3の中空部材による気液二相流冷媒の均一分
- 配・細分化現象を説明するための模式的断面図。 【図6】本発明の熱交換器を主体とする冷凍機の冷媒循
- 環システムの一部概要を示す模式図。 【図7】(A)は従来のプレート式熱交換器の一部省略 部分を含む正面図、(B)は側面図。
- 【図8】図7(A)のT2-T2線の拡大断面図。
- 【図9】図8の熱交換器の改変例を示す他の従来の熱交 換器の断面図。
- 【図10】図9の熱交換器に使用される金属リングの平 面図。

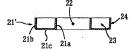
## 【符号の説明】

- 気液二相流冷媒
- 流体
- 伝熱プレート
- 冷媒用通路孔。 2
- 冷媒用流体流路
- 5 a 冷媒用入口流路 中空部材
- 流体流路

21

- 21' 中空部材
- 21a 内壁部
- 21b 外壁部
- 22 前段小孔
- 23 内部空間 後段小孔
- 24

[図4]

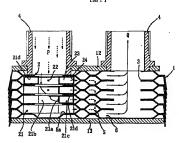


[図10]

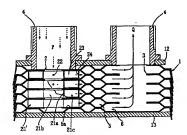


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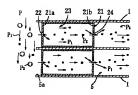
[図1]



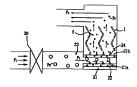
[図2]



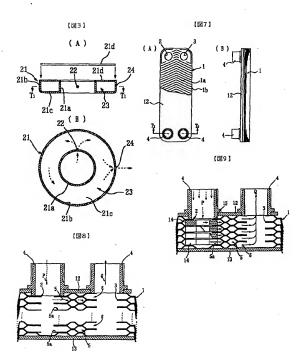
【図5】



[36]



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\* NOTICES \*

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3.In the drawings, any words are not translated.

#### DETAILED DESCRIPTION

[Detailed Description of the Invention]

[0001]

[Field of the Invention] This invention relates to the plate type heat exchanger which carried out the laminating unification of two or more heat transfer plates by soldering etc. 100021

Description of the Prior Art] Refrigerants, such as chlorofluocarbon of a refrigerator, serve as a gas from the heat exchanger of an evaporator 100%, serve as a liquid which sent and carried out the temperature rise to the condenser from a compressor, and are everlastingly used in the circulation cycle in which this liquid serves as vapor-liquid two-phases flow which the liquid phase (liquid) which carried out cubical expansion and carried out the temperature fall rapidly by the expansion valve, and a gaseous phase (air bubbles) mixed, and is sent to the heat exchanger of an evaporator. The heat exchanger used for the evaporator of the refrigerant of such a refrigerator has the common plate type heat exchanger which carried out the laminating unification of two or more heat transfer plates, the example of basic structure is shown in drawing 7 and drawing 8, and drawing 9 and drawing 10 explain the heat exchanger which changed this.

[0003] The heat exchanger shown in drawing 7 is a blazing type heat exchanger which carried out the laminating of the two metal frames 12 and 13 to two or more heat transfer plates 1 through wax material (not shown), and was soldered under the elevated temperature and the vacuum (blazing). The heat transfer plate 1 and the metal frames 12 and 13 are the abbreviation rectangle plates made from stainless steel, and the path holes 2 and 3 of two sorts of fluids by which heat exchange should be carried out are formed in four corners of each heat transfer plate 1, the nozzle 4 used as the entrance of two sorts of fluids makes four corners of one metal frame 12 penetrate, and they are soldered.

[0004] The heat transfer plate 1 has \*\*\*\*\*\*\* 1b which bent the periphery section of heat exchange heat transfer section 1a of a corrugated plate plate, and heat exchange heat transfer section 1a, and fused junction of the \*\*\*\*\*\*\* 1b of the adjoining heat transfer plate 1 is airtightly carried out by wax material. When the laminating unification of two or more heat transfer plates 1 is carried out, the path holes 2 and 3 formed in four corners of each heat exchange heat transfer section 1a counter this alignment, and are open for free passage. Moreover, when the laminating unification of two or more heat transfer plates 1 is carried out, as shown in drawing 8, the fluid passage 5 and 6 where two sorts of fluids whose one side is refrigerants circulate is formed by turns between each heat transfer plate 1. The cross section of the entrance side of the refrigerant P of the vapor-liquid two-phases flow whose drawing 8 is one sort of fluids, and the outlet side of one sort of other fluids O is shown, and the periphery path of the path hole 2 for refrigerants of the fluid passage 5 for refrigerants is inlet-port passage 5 for refrigerants a. Inlet-port passage 5a for refrigerants is the space part of the shape of a ring surrounded by the periphery of the entrance-side path hole 2 soldered at both the adjoining heat transfer plates 1. The entrance-side path hole 2 for refrigerants and the refrigerant P which flowed into the nozzle 4 open for free passage from the outside go into inlet-port passage 5a from the entrance-side path hole 2, and cools other fluids O which circulate the fluid passage 5 from inlet-port passage 5a, and circulate the next fluid passage 6. [0005] The refrigerant P which flows into inlet-port passage 5a of the fluid passage 5 for refrigerants is a vapor-liquid two-phases flow refrigerant of the liquid phase and a gaseous phase which the liquid condensed with the condenser which is not illustrated was expanded by the expansion valve, and was made to quench it, and the liquid phase and the gaseous phase of this vapor-liquid two-phases flow refrigerant repeat fission and coalesce, and it flows the fluid passage 5. In order to secure highly the total heat transfer engine performance of the refrigerant P which flows the fluid passage 5, the configuration

and size of inlet-port passage 5a are designed so that fragmentation of the homogeneity distribution of the gaseous phase of Refrigerant P and the liquid phase which go into the fluid passage 5 from inlet-port passage 5a, and the gaseous phase of the shape of a bubble with bad thermal conductivity may be promoted. However, in inlet-port passage 5a of only the clearance between the adjoining heat transfer plates 1, since Refrigerant P only passes, it cannot but be inferior to the function which promotes homogeneity distribution of a gaseous phase and the liquid phase, and fragmentation of a gaseous phase, and the total heat transfer engine performance of the refrigerant P in one fluid passage 5 cannot but become low. Then, although foresee this low heat transfer engine performance, the number of sheets of the heat transfer plate 1 is increased, the number of the fluid passage 5 for refrigerants is increased and he is trying to cover the total low heat transfer engine performance of a refrigerant, now, a heat exchanger is enlarged and it becomes cost quantity.

[0006] Since the total low heat transfer engine performance of the vapor-liquid two-phases flow refrigerant P of a heat exchanger is covered without increasing the number of heat transfer plates, in the plate type heat exchanger shown in drawing 9, the metal ring 14 of a thick plate as shown in inlet-port passage 5a for refrigerants at drawing 10 is fixed. A metal ring 14 is stainless steel, copper, or an iron thick plate, and a peripheral face is made to penetrate from inner skin, and it has the tunnel hole 15 of one articles. The bore of a metal ring 14 is the same as that of the path hole 2 for refrigerants of the heat transfer plate 1, or is smaller than it, and an outer diameter is larger than the path hole 2. A metal ring 14 is pinched between the adjoining heat transfer plates 1, and is positioned and fixed to the path hole 2 and this alignment. The tunnel hole 15 is a stoma with a bore of about 2mm which the refrigerant P of vapor-liquid two-phases flow is extracted, flows, and spreads and flows out.

[0007] In the heat exchanger of drawing 9, it is extracted to the tunnel hole inlet port of the inner circumference of a metal ring 14, and flows, and the vapor-liquid two-phases flow refrigerant P which flowed into the entrance-side path hole 2 for refrigerants flows, carries out the diffusion outflow of the tunnel hole 15 from the tunnel hole outlet of metal ring 14 periphery, and flows the fluid channel 5 for refrigerants. Thus, while the refrigerant P of vapor-liquid two-phases flow passes the tunnel hole 15 of a stoma, it is made for the total heat transfer engine performance of the refrigerant P at the time of flowing the fluid channel 5 for refrigerants to become high as the gaseous phase (air bubbles) of a comparatively big particle size of the refrigerant P of vapor-liquid two-phases flow is formed into homogeneity distribution by the small thing which it is subdivided granular and done for the rat tail diffusion of the flow of a gaseous phase and the liquid phase.

[0008]

[Problem(s) to be Solved by the Invention] Although the total heat transfer engine performance of Refrigerant P will be improved, the number of heat transfer plates will be lessened and small and low cost-ization of a heat exchanger will be realized if the heat exchanger of drawing 9 has homogeneity distribution of the vapor-liquid two-phases flow refrigerant P by the metal ring 14, and the good engine performance of fragmentation of a gaseous phase, the present condition is that the remarkable engineperformance improvement by the metal ring 14 is not yet achieved. As for fragmentation of a gaseous phase, as the factor, it is inadequate for one tunnel hole 15 of a metal ring 14 just to pass the vapor-liquid two-phases flow refrigerant P, possibility that an uneven and big gaseous phase will flow the fluid passage 5 is size, and this makes difficult the remarkable improvement of the total heat transfer engine performance. Moreover, although reducing the bore of the tunnel hole 15 of a metal ring 14, or increasing the number of tunnel holes, and considering as the remedy of the total heat transfer engine performance is also performed, it is difficult for the present condition for the improvement effect to be insufficient, and to lessen the number of heat transfer plates and to realize small and low cost-ization of a heat exchanger. [0009] This invention was made in view of the trouble of the heat exchanger of drawing 9, and the place made into the purpose is to offer the plate type heat exchanger which has improved notably the total heat transfer engine performance of a vapor-liquid two-phases flow refrigerant certainly. F00101

[Means for Solving the Problem] Invention of claim I which attains the above-mentioned purpose of this invention. The fluid passage where two sorts of fluids whose one side is vapor-liquid two-phases flow refrigerants circulate, and heat exchange is performed among two or more heat transfer plates by which the laminating was carried out is formed by turns. In the plate type heat exchanger which makes a refrigerant flow into the fluid passage for refrigerants from the inlet-port passage of the path hole circumference for inlet ports of the refrigerant formed in the heat transfer plate. The preceding paragraph stoma out of which the flow is extracted to the inlet-port passage of the fluid passage for refrigerants, and the vapor-liquid two-phases flow refrigerant from the outside flows into it, and spreads and flows into it.



and the building envelope where the refrigerant which flowed out carries out reduced pressure expansion of this preceding paragraph stoma -- and That flow is extracted, and the refrigerant which carried out reduced pressure expansion in this building envelope arranges the centrum material which has the latterpart stoma which flows, and spreads and flows out, and is characterized by making a refrigerant flow into the fluid passage for refrigerants from the latter-part stoma of this centrum material. [0011] Here, centrum material is metal boxes, such as the shape of a ring which takes up the inlet-port passage of the fluid passage for refrigerants, and a metal vessel, and is fixed to a heat transfer plate by soldering, welding, etc. To refrigerant flow, it has a preceding paragraph stoma in the upstream, it has a latter-part storna in the downstream, as for this centrum material, a building envelope is formed between the stomata of an order [ this ] stage, and, finally the refrigerant of vapor-liquid two-phases flow flows out and goes to fluid passage from a latter-part stoma through a building envelope from a preceding paragraph storna. A single hole or two or more holes are possible for each stoma of the preceding paragraph of centrum material, and the latter part, and the bore of these stomata and its include angle of a hole center line are also arbitrary, there is, and it is suitably set up according to the class of heat exchanger. Moreover, the building envelope of centrum material may be single space or two or more space which were divided into the fluid flow direction serial with the bridge wall, in the case of these two or more space, an in-between stoma is formed in the bridge wall which divides two or more space, and it pours a refrigerant in order to two or more space. Homogeneity distribution of the final gaseous phase and the liquid phase of a vapor-liquid two-phases flow refrigerant and fragmentation of a gaseous phase are notably ensured by the refrigerant of vapor-liquid two-phases flow having two or more stomata extracted. and circulating, and refrigerant circulation of a different gestalt of carrying out reduced pressure expansion and flowing out of a stoma into a building envelope covering multiple times further, and being carried out gradually and in repeat.

[0012] Centrum material has the shape of a ring which has the outer wall section of a major diameter from cylinder-like the wall section and this wall section of a minor diameter, and invention of claim 2 of this invention is characterized by forming [a preceding paragraph stoma ] a building envelope in the wall section for a latter-part stoma between the wall section and the outer wall section in the outer wall section. The appearance of this ring-like centrum material is the same as that of the conventional metal ring, and is fixed in the form pinched by the periphery of the refrigerant inlet-port passage hole of an adjoining heat transfer plate. While the refrigerant which flowed into the refrigerant inlet-port passage hole of a heat transfer plate passes through the inside of the wall section of ring-like centrum material, some refrigerants

flow into a preceding paragraph stoma.

[0013] Invention of claim 3 of this invention makes centrum material pinch through wax material on an adjoining heat transfer plate, and is characterized by carrying out soldering immobilization between heat transfer plates. Thus, if centrum material is soldered on a heat transfer plate, at the time of manufacture of the blazing type heat exchanger which solders two or more heat transfer plates, at the same process as soldering of two or more heat transfer plates, soldering of centrum material can be performed and manufacture of a heat exchanger will be carried out in favor of a process cost target.

[0014]

[Embodiment of the Invention] Hereafter, the operation gestalt of this invention is explained in full detail with reference to drawing 1 thru/or drawing 6. In addition, this operation gestalt is what was applied the heat exchanger of drawing 8 or drawing 9, the same reference mark is given to drawing 7 of drawing 1 thru/or drawing 6 thru/or drawing 9, the same, or a considerable part, and that detail explanation is comitted

[0015] The heat exchanger of the 1st operation gestalt shown in drawing 1 is a plate type heat exchanger of a blazing type, and fixes the centrum material 21 to each of inlet-port passage 5a of two or more fluid passage 5 for refrigerants formed among two or more heat transfer plates 1. The centrum material 21 is metal goods, such as stainless steel of the shape of a ring as shown in drawing 3, it has cylinder-like wall section 21a and outer wall section 21b, and the preceding paragraph stoma 22 is formed in one place of wall section 21a, the latter-part stoma 24 is formed in one place of outer wall section 21b, and the building envelope 23 of the letter of sealing is formed between wall section 21a and outer wall section 21a. Each stornata 22 and 24 of an order stage are through tubes with a bore of about 2mm which the refrigerant P of vapor-liquid two-phases flow is extracted, and circulates.

[0016] the centrum material 21 shown in drawing 1 and drawing 3 -- among those, wall 21a is smaller than the bore of the inlet-port passage hole 2 for refrigerants of the heat transfer plate 1 -- it is cylindrical and outer wall section 21b is bigger than the bore of the inlet-port passage hole 2 -- it is cylindrical and the lower limit of wall section 21a and outer wall section 21b is connected with one by ring-like bottom

plate section 21c. The centrum material 21 consists of the upper limit opening ring-like container which consists of this wall section 21a, outer wall section 21b, and bottom plate section 21c being manufactured by press working of sheet metal or cutting, and sealing upper limit opening of this ring-like container by 21d of metaled ring-like cover plates. 21d of cover plates is the space sealing lid which prevents that the refrigerant P of vapor-liquid two-phases flow does not pass along the preceding paragraph stoma 22, but flows into a building envelope 23 directly, and they are unnecessary for such a lid in the 2nd operation gestalt of drawing 2, are omitted, and mention the reason later.

[0017] The ring-like centrum material 21 is positioned so that the center line of the inlet-port passage hole 2 and the center line of wall section 21a may be mostly in agreement with the periphery of the inlet-port passage hole 2 for refrigerants of the adjoining heat transfer plate 1, and it is fixed by immobilization, for example, soldering. Thus, if the centrum material 21 is soldered on the heat transfer plate 1, soldering of heat transfer plates and soldering of the centrum material 21 can perform at one process at the time of manufacture of the blazing type heat exchanger which solders heat transfer plates, and will become advantageous [manufacture of a blazing type heat exchanger / process ] in cost at it. The ring-like centrum material 21 turns the latter-part stoma 24 in the direction of the fluid passage 5 for refrigerants. and is fixed to inlet-port passage 5a for refrigerants. Although the directivity of the preceding paragraph stoma 22 of this centrum material 21 is not limited, it is made to be located in the 90-degree constant

direction to the latter-part stoma 24, as shown in drawing 3.

[0018] If two or more ring-like centrum material 21 is fixed to two or more inlet-port passage 5a for refrigerants between two or more heat transfer plates 1 and the vapor-liquid two-phases flow refrigerant P is made to flow from the refrigerant inlet-port nozzle 4, the wall section 21a inner skin of each ring-like centrum material 21 will be flowed to shaft orientations, some refrigerants P will be extracted to the preceding paragraph stoma 22 of wall section 21a, and Refrigerant P will flow into a building envelope 23. This refrigerant inflow is performed as shown in drawing 5. Although the refrigerant P of the vaporliquid two-phases flow which flows the outside of wall section 21a is the gaseous phase (air bubbles) P2 shown by the particle conceptual diagram of the liquid phase P1 shown by the conceptual diagram of the continuous-line arrow head of drawing 5, and drawing 5, its particle size of a gaseous phase P2 is comparatively large, and the heat transfer engine performance will fall if this is made to flow into the fluid passage 5 for refrigerants as it is temporarily The liquid phase P1 and a gaseous phase P are made to flow into a building envelope 23 from the preceding paragraph stoma 22 first in this invention. In order to carry out reduced pressure expansion when flowing out of the preceding paragraph stoma 22 into a building envelope 23 while being extracted and diameter of a granule 1-ized, when the gaseous phase P2 with a big particle size passes to the preceding paragraph stoma 22, in a building envelope 23, a gaseous phase P2 and the liquid phase P1 are formed into homogeneity distribution, and most gaseous phases P2 are subdivided in the shape of a granule child.

[0019] Furthermore, the refrigerant P which flowed into the building envelope 23 from the preceding paragraph stoma 22 flows the ring-like building envelope 23, as shown in drawing 3 (B), finally it is extracted to the latter-part stoma 24, flows, and flows out and goes to the fluid passage 5 for refrigerants. Also in the phase where Refrigerant P passes the latter-part stoma 24, the formation of homogeneity distribution and gaseous-phase fragmentation of the gaseous-phase liquid phase are performed. The gaseous-phase fragmentation by this latter-part stoma 24 is that the gaseous phase of a particle while [ comparatively big ] flowing from the preceding paragraph stoma 22 to the building envelope 23, and the gaseous phase of a particle while coalescing between the short time which flows a building envelope 23 are subdivided in the shape of a granule child.

[0020] As mentioned above, by the centrum material 21, the vapor-liquid two-phases flow refrigerant P is an operation of the reduced pressure expansion covering two steps by the homogeneity distribution of the gaseous-phase liquid phase and the gaseous-phase fragmentation covering two steps by two steps of stomata 22 and 24, the outflow to a building envelope 23 from the preceding paragraph stoma 22, and the outflow to the space of the fluid passage 5 from the latter-part stoma 24 approximately, and homogeneity distribution and gaseous-phase fragmentation of the gaseous-phase liquid phase are performed certainly and notably, and it circulates the fluid passage 5. Therefore, it improves certainly, and the total heat transfer engine performance of the refrigerant P in one fluid passage 5 lessens the number of heat transfer plates, miniaturizes a heat exchanger, and turns into that manufacturing by low cost is possible. [0021] The refrigerant P which drawing 6 is a schematic diagram when applying the heat exchanger of drawing 1 to the refrigerant circulation system of a refrigerator, and is sent from a condenser (not shown) has the liquid phase P1 in use, this serves as the vapor-liquid two-phases flow refrigerant P of the liquid phase P1 and a gaseous phase P2 by the expansion valve 30, and is sent to a heat exchanger, and reaches

the internal centrum material 21. This refrigerant P flows into a building envelope 23 from the preceding paragraph stoma 22 of wall section 21a of two or more centrum material 21, flows out of the latter-part stoma 24 of outer wall section 21b, and flows the fluid passage 5. In this case, in order that the refrigerant P of vapor-liquid two-phases flow with which the homogeneity distribution of the gaseous-phase liquid phase were fully carried out, and the gaseous phase P2 was subdivided may flow the fluid passage 5 between the heat transfer plates 1, efficient heat exchange is performed and an advanced refrigerating cycle is realized. Most serves as a gaseous-phase component, and the refrigerant P which came out of the heat exchanger is sent to a consecutive compressor, is sent to a condenser and an expansion valve from a compressor, and returns to a heat exchanger.

[0022] The heat exchanger of the 2nd operation gestalt shown in drawing 2 shows the example of a structural change of the above-mentioned centrum material 21, and centrum material 21' in drawing 2 is the ring-like metal vessel of an upper limit opening owner bottom without a lid as shown in drawing 4. This centrum material 21' consists of only cylinder-like wall section 21a, outer wall section 21b, and ringlike bottom plate section 21c, the preceding paragraph stoma 22 is formed in one place of wall section 21a, the latter-part stoma 24 is formed in one place of outer wall section 21b, and between wall section 21a and outer wall section 21b turns into a building envelope 24.

[0023] Centrum material 21' of drawing 2 was made to correspond to the geometry of refrigerant inletport passage 5a to which this is fixed, and the bore of wall section 21a of centrum material 21' is more greatly set up from the bore of the path hole 2 for refrigerants of refrigerant inlet-port passage 5a in this case. Therefore, if centrum material 21' without a lid is positioned to refrigerant inlet-port passage 5a and it fixes, since upper limit opening of the centrum material 217 will be closed by the periphery of the path hole 2 of the heat transfer plate 1 and a building envelope 23 will turn into an abbreviation closed space, this centrum material 21' does not need a cover plate. The function of the gaseous-phase liquid phase homogeneity decentralization to the vapor-liquid two-phases flow refrigerant P of such lid-less centrum material 21' or gaseous-phase fragmentation omits explanation like the centrum material 21 with a lid of drawing 3 therefore.

[0024] Although centrum material was made into the shape of a ring in each above operation gestalt, this could be made to correspond to the ring-like inlet-port passage for refrigerants, and can be made into the configuration of the arbitration according to the configuration of the inlet-port passage for refrigerants, for example, may be the centrum material of a semicircle arc etc. Moreover, although the preceding paragraph stoma was formed in one place of the wall section of centrum material and the latter-part stoma was formed in one place of the outer wall section, the number of each [ these ] stoma, magnitude, a configuration, and a formation location are not pinpointed. Moreover, although one building envelope was formed between the wall section of centrum material, and the outer wall section, a refrigerant carries out reduced pressure expansion of two or more space where the batch was divided into plurality in this building envelope at order, and you may make it flow.

100251 Furthermore, this invention is applied effective in the plate type heat exchanger of gasket seal types other than a blazing type heat exchanger etc., carries out the pressure welding of the centrum material to a heat transfer plate through immobilization or a gasket at a heat transfer plate in a gasket seal type heat exchanger by welding, and should just fix it.

[Effect of the Invention] According to invention of claims 1 and 2, the refrigerant of vapor-liquid twophases flow The preceding paragraph stoma of centrum material, Since a building envelope and a latterpart stoma are passed in order, homogeneity distribution of the gaseous-phase liquid phase and fragmentation of a gaseous phase are performed to at least two steps for the time of this passage and it flows into the fluid passage for refrigerants The gaseous-phase liquid phase homogeneity distribution and the gaseous-phase fragmentation of a refrigerant in fluid passage are performed sufficiently notably, the total heat transfer engine performance of a refrigerant improves, and the plate type heat exchanger excellent in heat exchange effectiveness can be offered. Moreover, it becomes easy to lessen the number of heat transfer plates, to make a heat exchanger into a small light weight, and to reduce manufacture cost by improvement of the total heat transfer engine performance of a refrigerant.

[0027] According to invention of claim 3, by fixing centrum material by soldering between adjoining heat transfer plates, centrum material can be fixed to the existing heat transfer plate by the existing soldering approach, without the blazing type heat exchanger soldered to coincidence being able to manufacture two or more heat transfer plates by soldering of one process, and using another member with a special gasket etc., and the advantageous plate type heat exchanger in manufacture can be offered.



- [Translation done.]



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#### DESCRIPTION OF DRAWINGS

[Brief Description of the Drawings]

[Drawing 1] The sectional view of the important section of a plate type heat exchanger showing the 1st operation gestalt of this invention.

[Drawing 2] The sectional view of the important section of a plate type heat exchanger showing the 2nd operation gestalt of this invention.

[Drawing 3] For (A), the sectional view of the centrum material in the drawing 1 heat exchanger and (B) are the sectional view of T1-T1 line.

[Drawing 4] The sectional view of the centrum material in the drawing 2 heat exchanger.

[Drawing 5] The typical sectional view for explaining homogeneity distribution / fragmentation

phenomenon of the vapor-liquid two-phases flow refrigerant by the centrum material of drawing 3.

[Drawing 6] The refrigerant circulation system of the refrigerator which makes the heat exchanger of this invention a subject is the mimetic diagram showing an outline a part.

[Drawing 7] (A) is a front view of the conventional plate type heat exchanger which contains an

abbreviation part in part, and (B) is a side elevation.

Drawing 81 The expanded sectional view of T2-T2 line of drawing 7 (A).

[Drawing 9] The sectional view of other conventional heat exchangers showing the example of an alteration of the heat exchanger of drawing 8.

Drawing 101 The top view of the metal ring used for the heat exchanger of drawing 9.

[Description of Notations]

P Vapor-liquid two-phases flow refrigerant

O Fluid

1 Heat Transfer Plate

2 Path Hole for Refrigerants

5 Fluid Passage for Refrigerants

5a Inlet-port passage for refrigerants

6 Fluid Passage

21 Centrum Material

21' Centrum material

21a Wall section

21b Outer wall section

22 Preceding Paragraph Stoma

23 Building Envelope

24 Latter-Part Stoma

[Translation done.]





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## CLAIMS

[Claim(s)]

[Claim 1] The fluid passage where two sorts of fluids whose one side is vapor-liquid two-phases flow refrigerants circulate, and heat exchange is performed among two or more heat transfer plates by which the laminating was carried out is formed by turns. In the plate type heat exchanger which makes a refrigerant flow into the fluid passage for refrigerants from the inlet-port passage of the path hole circumference for inlet ports of the refrigerant formed in the heat transfer plate The preceding paragraph stoma out of which the flow is extracted to the inlet-port passage of the fluid passage for refrigerants, and the vapor-liquid two-phases flow refrigerant from the outside flows into it, and spreads and flows into it, and the building envelope where the refrigerant which flowed out carries out reduced pressure expansion of this preceding paragraph stoma -- and The plate type heat exchanger to which the refrigerant which carried out reduced pressure expansion in this building envelope is characterized by extracting that flow, arranging the centrum material which has the latter-part stoma which flows, and spreads and flows out, and making a refrigerant flow into the fluid passage for refrigerants from the latter-part stoma of this centrum material.

[Claim 2] centrum material -- the wall section of a cylinder-like minor diameter -- among these, the plate type heat exchanger according to claim 1 characterized by forming [a preceding paragraph stoma] a building envelope for a latter-part stoma between the wall section and the outer wall section in the wall section at the outer wall section by the shape of a ring which has the outer wall section of a major diameter from a wall.

[Claim 3] The plate type heat exchanger according to claim 1 or 2 characterized by having made centrum material pinch through wax material on an adjoining heat transfer plate, and carrying out soldering immobilization between heat transfer plates.

[Translation done.]

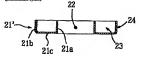
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## DRAWINGS

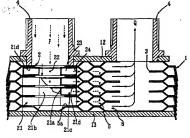
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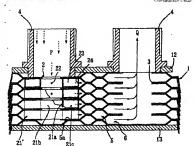
## [Drawing 10]

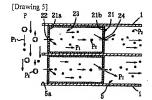


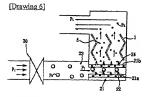
# [Drawing 1]



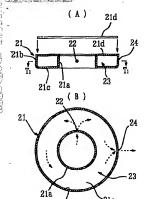
[Drawing 2]

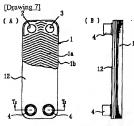


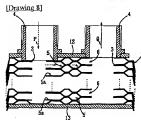




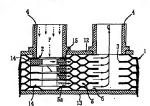
[Drawing 3]







[Drawing 9]



[Translation done.]